

## **AMENDMENTS TO THE SPECIFICATION:**

On page 4, please replace the paragraph starting on line 30 with the following replacement paragraph:

- -The crux of the invention is the feature of putting into place a significantly stronger cooling of the casting die body in the supercritically stressed areas on both sides of the funnel. According to the invention, it is proposed to increase the cooling capacity in these critical areas preferably 10 to 20% in relation to the horizontal adjoining areas. Coolant channels 6 (Figures 4 and 5), for example, can be advantageously made narrower here (Figure 4), so that the cooled surface is made larger. Alternatively, the coolant channels 6 can be brought closer to the surface locally (Figure 5); in this case, the system operates, in an unusual fashion, with varying -- effectively active -- cooling wall thicknesses above the cooling water. The same applies to cooling bore holes 14 (Figure 3). In addition, broad-side plates, configured having groove-shaped coolant channels 6, in the critical areas of the funnel transition can be provided with additional cooling bore holes 14; in a surprising manner, in spite of the small wall thickness, the resistance to cracks of the casting die material is increased also here and with it the overall durability of the casting die plate.- -.

On page 4, please add the following paragraph starting on line 30:

- -The casting die body has, running parallel to the pouring direction, a groove-shaped coolant channel or cooling bore holes, which in the thermally and mechanically stressed areas are configured narrower. The cooling bores are arranged between the coolant channels.- -.

On page 5, please replace the paragraph starting on line 27 with the following replacement paragraph:

- -Funnel casting die plate 1, represented in Figure 1, in the horizontal dimension (vertical line C) of funnel 2 on a pouring side 4, has the highest thermal stressing. A direct consequence is a maximum surface-related heat flow of 4.7 to 5.2 and MW/m<sup>2</sup> lying directly beneath bath surface 3 at C in the pouring direction [[GR]] PD. Present on pouring side 4 of casting die plate 1 are maximum temperatures of approximately 400°C, calculated by computer. Actively effective wall thickness d of casting die plate 1

of copper is now reduced in critical area 5 between the lines B, C, and D, to the upper 200 mm of the casting die plate from  $d_1 = 20$  mm to  $d_2 = 18$  mm (Figures 4 and 5).- -.